# Critical Properties and Vapor-Liquid Equilibria of the Binary System Propane + Neopentane

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Vapor-liquid equilibrium data extending to critical pressures are reported for five mixtures of propane with neopentane. The data in pressure, temperature, and density are correlated to high accuracy by the Leung-Griffiths model as modified by Moldover, Rainwater, and co-workers. In addition, a complete bibliography of similar experiments on binary mixtures from the laboratory of W.B.K. is presented.

### Introduction

Recently, several papers (1-6) have appeared which have included hitherto unpublished vapor-liquid equilibrium (VLE) data from the Ohio State University laboratory, together with correlations based on classical equations of state. The experiments described in those papers consisted of measurements of dew-bubble curves in pressure (P), temperature (T), and (in most cases) density ( $\rho$ ) along isopleths or loci of fixed mole fraction (x) for a selected set of binary mixtures. A large number of dew and bubble points have been measured very near the critical locus of each mixture, so the critical regions have been very well characterized.

In this paper and the following one (7) we present some additional, hitherto unpublished VLE data from the Ohio State laboratory. Furthermore, we correlate these measurements by a relatively new thermodynamic technique, the Leung-Griffiths model (8) as modified by Moldover, Gallagher, and Rainwater (9-13), which is specifically designed to be accurate within the critical region. This model has been successful in correlating more than 40 binary mixtures (9-17) and has consistently led to excellent agreement with the experiments of Kay and co-workers in particular (14, 16).

The subject of this first paper is the binary mixture of propane with neopentane (2,2-dimethylpropane or tetramethylmethane) as measured by Hissong (18). The following paper (7) examines binary mixtures of propane with each of the five isomers of hexane, as measured by Chun (19). When combined with correlations of the propane + *n*-pentane mixture (13, 20, 21), and of the propane + isopentane mixture (14, 22), accurate data and correlations are now available for all mixtures of propane with alkanes of five or six carbon atoms.

Table I summarizes the VLE experiments of Kay and coworkers that are amenable to correlation with the modified Leung-Griffiths theory. As a general policy, before 1980 smoothed data (at even intervals of pressure) were presented in archival journals, whereas original or raw data were preserved in theses and, in most cases, made available through an auxiliary publication serivce. The unpublished industrial reports and M.Sc. theses cited in Table I are only available from the respective institutions, but J.C.R. is developing a comprehensive database with original data from these sources

<sup>†</sup> Present address: Exxon Production Research Corp., P.O Box 2189, Houston, TX 77001. and from other laboratories, and can provide data files or tables upon request.

The table excludes studies of binary mixtures such as benzene + water (73) and helium + n-butane (74) which have discontinuous critical loci and therefore cannot be correlated by the modified Leung-Griffiths model. Also excluded, for the most part, are a large number of studies in which dew and bubble points (usually without densities) were measured only very close to the critical locus; several such papers have already been cited (4, 6, 69). The primary objective of this second class of experiments was to determine the critical locus rather than the coexistence surface. In all of the experiments cited in Table I, the fluids were subjected to a degassing process in which dissolved air was carefully removed, as described below. However, for the second class of experiments, the fluids in some cases were not degassed.

In a series of three papers, Kay and Hissong (75-77) have presented graphically data from the second class of experiments for 50 hydrocarbon mixtures. Original data are tabulated in the theses cited therein, except for those from the thesis of Hissong (78) which are only available in graphical form. Similar papers, with original data available from the theses cited therein, are by Kay (70) on acetone + n-alkane mixtures, by Kreglewski and Kay (51), and by Mousa *et al.* (79). Pak and Kay (80) have reported direct critical locus measurements on 15 additional hydrocarbon mixtures. Finally, in the study of carbon dioxide + benzene and sulfur dioxide + benzene by Kay and Kreglewski (81), the critical loci were measured directly but the dew and bubble curves reported there were inferred from an equation of state rather than measured.

Propane + neopentane is one of a relatively few number of neopentane mixtures for which data on phase equilibrium are available in the critical region. VLE data that span the full phase diagram have been presented for mixtures of neopentane with carbon dioxide (82, 83) and tetramethylsilane (84). More limited studies provide VLE along critical isotherms for mixtures of neopentane with methane (85, 86), argon (85, 87), hydrogen sulfide (88), and carbon tetrafluoride (89), and along isopleths for mixtures of neopentane with *n*-pentane and cyclopentane (90). In addition, critical temperature loci have been measured for mixtures of neopentane with *n*-pentane, *n*-hexane, cyclohexane, benzene, and toluene (91).

While the modified Leung-Griffiths model does show promise for correlating limited VLE data (15), it is best applied

#### Journal of Chemical and Engineering Data, Vol. 38, No. 4, 1993 487

Table I.	VLE ]	Bibliogra	ohy of l	Kay and	Co-workers
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		reference				
	mixture	original data	smoothed data	critical locus	number of isopleths	
1	ethane $+ n$ -heptane	23	24	24	5	
2	ethane + n-butane	25	26	26	5	
3	<i>n</i> -butane + <i>n</i> -heptane	27	28	28	5	
4	ethylene + n-heptane	29	30	30	8	
5	ethane + benzene	31	32	32	7	
6	propane + hydrogen sulfide <sup>a</sup>	33	34	34	7	
7	ethane + hydrogen sulfide <sup>a</sup>	35	36	36	6	
8	carbon dioxide + hydrogen sulfide	37	38	38	8	
9	methanol + 1-butanol	39	40	40	4	
10	diethyl ether + 1-butanol	39	40	40	4	
11	isobutanol + 1-butanol	39	40	40	3	
12	ethane + cyclohexane	41	42	42	6	
13	ammonia $+ n$ -butane <sup>a</sup>	43	44 <sup>b</sup>	44	6	
14	ammonia + isooctane <sup><math>\alpha</math></sup> (2.2.4-trimethylpentane)	45°	46	46	11	
15	methanol + henzene	47	48	48	5	
16	ethanol + benzene	47	48	48	7	
17	1-propenol + benzene	47	48	48	7	
18	1-butenol + benzene	47	48	48	Ġ	
10	$r_{onene} + n_{onene}$	40	50	51 50	5	
20	$\mathbf{p} \mathbf{o} \mathbf{p} \mathbf{a} \mathbf{n} \mathbf{e} + n \mathbf{e} \mathbf{p} \mathbf{a} \mathbf{n} \mathbf{e}$	59	50	51,50	5	
20	propane $+ n$ -pentane	52	54	51,50	5	
21	propane $+ n$ herene	7 10	04	7 55	5	
99	propane $\pm 2$ -methylaentene	7,19		7,55	5 5	
44 00	propane $\pm 2$ methylpentane	7,19		7,55	5	
20	propane + $3.9$ dimethylbutane	7,19		7,55	5 E	
24 05	propane + $2,2$ -dimethylbutane	7,19		7,00	5 E	
20	propane + 2,3-dimethylbutane	7,19	54	7,00 51 54	9 E	
20	propane + $n$ -neptane	50	04 50	01, 04 51 59	0 6	
27	propane + n-octane	07 50	00 F0	01, 08 FO	6	
28	<i>n</i> -butane + <i>n</i> -octane	09	00 01	00 01	5	
29	n-butane $+ n$ -pentane	00	01	61	5	
30	n-Dutane $+ n$ -nexane	62	61	61	6	
31	(perfluoromethyl)cyclonexane (PFMCH) + n-nexane	63, 1		64	b	
32	PFMCH + 2-methylpentane"	63, 1		64	6	
33	PFMCH + 3-methylpentane"	63, 1		64	6	
34	PFMCH + 2,2-dimethylbutane <sup>a</sup>	63, 1		64	6	
35	PFMCH + 2,3-dimethylbutane"	63, 1		64	6	
36	perfluorocyclobutane + n-propane <sup>a</sup>	65, 2		66	7	
37	pentane + pent-1-ene	67, 3		67, 3	3	
38	acetone + $n$ -pentane <sup>a</sup>	68, 5		5	5	
	acetone + $n$ -pentane <sup>a</sup>	69, <sup>a,e</sup> 5		70	5	
39	propane + neopentane	18		18	5	
40	ethane + perfluoro-n-heptane	71*		72	5	
41	propane + perfluoro- <i>n</i> -heptane	71^		72	6	
42	<i>n</i> -butane + perfluoro- <i>n</i> -heptane <sup>a</sup>	71		72	6	
43	<i>n</i> -pentane-perfluoro- <i>n</i> -heptane <sup>a</sup>	71		72	6	
44	<i>n</i> -hexane + perfluoro- <i>n</i> -heptane <sup>a</sup>	71		72	7	
45	n-heptane + perfluoro-n-heptane <sup>a</sup>	71		72	10	
46	<i>n</i> -octane + perfluoro- <i>n</i> -heptane	71 <sup>e</sup>		72	8	
47	<i>n</i> -nonane + perfluoro- <i>n</i> -heptane	$71^{h}$		72	6	

<sup>a</sup> Azeotropic mixtures. <sup>b</sup> Smoothed in composition as well as pressure. <sup>c</sup> Also contains liquid-liquid equilibrium data. <sup>d</sup> coexisting density data absent. <sup>e</sup> Liquid and vapor data all very close to critical locus. <sup>f</sup> Coexisting liquid density data absent. <sup>g</sup> This paper. <sup>h</sup> Liquid data all very close to critical locus.

to experiments such as those listed in Table I with coexisting density data and dew-bubble curves over a wide range of pressures. As seen from Table I, with the publication of this paper and the following one, data from all of the more thorough studies of Kay and co-workers are now available in the archival literature, except for those of Jordan (71). Attempts to correlate Jordan's data with the modified Leung-Griffiths model are currently in progress; these efforts are complicated by the presence of azeotropy and some peculiar features of hydrocarbon + fluorocarbon mixtures. A similar publication based on Jordan's data is planned, pending some further analysis.

#### **Apparatus and Experimental Data**

The apparatus used in this work was, for the most part, identical to that described by Kay and Rambosek (34). Figure 1 presents a schematic diagram of this apparatus, each component of which will be referred to in the following.

The hydrocarbon sample was confined over mercury in a thick-walled glass capillary tube (a) of approximately 3-mm bore, which was mounted in a compressor block (b) and surrounded by a vacuum-insulated heating jacket (c). The temperature was maintained by boiling a pure organic compound in the side arm flask (d) connected to the bottom of the jacket. A stream of air was blown across the jacket near its top (e) to condense the vapors of the boiling compound. The top of the heating jacket was connected through a water condenser (f) to a mercury manometer (g) and a series of large containers (h) which provided a surge volume of about  $0.057 \text{ m}^3$  (57 L). The pressure in this system was controlled by allowing air to pass through two 100-mL bulbs, one of which was connected to a vacuum pump (i) and the other was open to the atmosphere (j). By varying the boiling pressure within the jacket in this manner, we could control the sample temperature very precisely.



Figure 1. Apparatus to measure phase equilibrium in pressure, volume, and temperature.

The sample temperature was measured with a copperconstantan thermocouple (k), which was inserted into the top of the heating jacket. The tip of the thermocouple was about 1 cm above the closed end of the sample tube, and the cold junction was kept in a Dewar flask containing an icewater mixture. The thermocouple emf was measured with a precision potentiometer. The thermocouple was calibrated by comparing it with a platinum resistance thermometer, which had been certified by the National Bureau of Standards.

Pressure was transmitted to the sample through mercury in the U-shaped compressor block. Compressed nitrogen from a cylinder (1) entered a manifold (m) to which were connected a 1-L surge tank (n) and a precision Bourdon gauge (o), which was calibrated by comparison with a dead weight gauge. The manifold was connected to the back leg of the compressor block. Through the double valve systems on the high-pressure nitrogen inlet and the exhaust line (p) of the manifold, small quantities of nitrogen could be added to, or removed from, the system. In this way, the pressure of the sample could be precisely controlled.

The sample volume was measured by determining the position of the interface in the capillary tube with a precision cathetometer. The volume of the tube was known as a function of the distance from the closed end by a previous calibration. Several mercury levels were also measured for use in calculating the sample pressure. The sample in the capillary tube was stirred by moving a steel ball within the tube by means of a strong magnet held outside the heating jacket.

The propane and neopentane used in this work were highpurity research-grade materials. They were degassed (freed of dissolved air) by a cyclic operation which involved freezing, pumping off released gas, melting, and distillation at low pressure. They were then sealed into glass ampules. The experimental tube was filled with mercury while attached to a vacuum train and under high vacuum. The propane and neopentane were charged to the tube by mercury displacement. The critical properties of both pure components were measured and compared with published values as a check on the methods used and the purity of the hydrocarbons.

 Table II. Critical Properties of Binary Systems of

 Neopentane (1) + Propane (2)

	-				
$T_{\rm c}({\rm K})$		$P_{\rm c}$ (1	/Pa)	$ ho_{\rm c}~({\rm kg/m^3})$	
exptl	fit	exptl	fit	exptl	fit
426.46	426.641	3.4798	3.4783	232.8	230.44
410.32	410.319	3.9436	3.9461	230.7	228.14
396.96	396.960	4.1903	4.1869	230.0	227.26
385.88	385.882	4.2855	4.2883	227.7	226.19
375.71	375.707	4.2936	4.2923	221.7	223.51
	Tc           exptl           426.46           410.32           396.96           385.88           375.71	T <sub>c</sub> (K)           exptl         fit           426.46         426.641           410.32         410.319           396.96         396.960           385.88         385.882           375.71         375.707	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$

Compositions of the mixtures were determined from measured component volumes and known densities. Details of these procedures have been described by Kay and Rambosek (34). The measured pressures were corrected by subtracting the vapor pressure of mercury at the measured temperature. The magnitude of the corrections for mercury vapor dissolved in hydrocarbon mixtures has been analyzed by Kay and Pak (92); at the temperatures of this study such corrections are very small.

Five mixtures of propane and neopentane were studied. The pressure, temperature, and volume at the bubble and dew points were measured over a temperature range from approximately 350 K to the maximum temperature at which liquid and vapor coexist. The critical point was determined visually as the conditions at which the meniscus between the vapor and liquid phases disappeared. Measured critical points are listed in Table II.

Dew and bubble points for the propane + neopentane mixture are listed in Table III and are displayed in the P-Tplot of Figure 2 and the  $T-\rho$  plot of Figure 3. Also shown in the figures are the pure-fluid coexistence loci, the critical locus, and the predictions of the modified Leung-Griffiths model as discussed in the following sections. Clearly the data are highly self-consistent, in that they form smooth curves with no evidence of scatter on the scale of the figures. Also, the region close to the critical point has been thoroughly investigated, as is evident from the figures.

The precision of the data is estimated to be as follows: temperature, 0.1 K; pressure, 0.014 MPa (2.0 psi); density,  $1.0 \text{ kg/m}^3$  for the liquid and  $0.1 \text{ kg/m}^3$  for the vapor. However, in the critical region, the uncertainty in the values reported

P (MPa)	<i>T</i> (K)	ho (g/cm <sup>3</sup> )	P (MPa)	<i>T</i> (K)	ho (g/cm <sup>3</sup> )
		$x_2 = ($	0.1581		
1.1342	357.48	0.497 37	2.2977	404.11	0.076 88
1.2426	362.11	0.491 04	2.6728	407.45	0.390 74
1.3486	366.55	0.482 00	2.4384	407.45	0.083 84
1.4346	370.08	0.475 99	2.7947	410.51	0.379 92
1.5285	373.62	0.470 34	2.5683	410.51	0.091 48
1.6073	376.31	0.465 80	2.9452	413.75	0.367 80
1,6991	379.55	0.458 93	2,7280	413.75	0.100.06
1 7800	382.28	0 452 82	3 0878	417 14	0.353.40
1.8706	385 15	0 448 54	2 8934	417 14	0 111 49
1 6999	385 91	0.040 90	3 9056	410.03	0.225.07
1.0002	300.21	0.045 35	3.2000	410.04	0.000 51
1.0900	300.00	0.440 20	0.0000	419.94	0.123 00
1.0005	300.00	0.000 17	0.1510	422.23	0.319 00
1.9711	366.30	0.441 00	3.1019	422.23	0.136 25
1.7331	388.30	0.003 01	3.3847	423.71	0.306 06
2.1025	392.35	0.431 34	3.2394	423.71	0.147 19
1.8659	392.35	0.058 16	3.4274	424.69	0.294 72
2.2189	395.67	0.423 57	3.3001	424.59	0.155 30
1.9823	395.67	0.063 17	3.4708	425.58	0.276 93
2.3273	398.70	0.415 29	3.3654	425.58	0.167 91
2.0953	398.70	0.067 65	3.4792	426.13	0.257 57
2.4248	401.32	0.409 51	3.4068	426.13	0.179 31
2.1923	401.33	0.071 91	3.4798	426.46	0.232 81
2.5353	404.11	0.400 25	-	-	
		*• = (	4573		
1.9205	361.27	0.458.07	3,4406	406.16	0.124 65
2 0357	364 67	0 451 30	3 0001	408.03	0.289.97
9 1955	360 06	0.401 50	9 KONK	100.05	0.200 01
2.1000	279.08	0.499.45	3.0000	400.07	0.137.35
2.3340	372.90	0.400.01	0.7001	409.01	0.201 99
2.4909	377.13	0.423 91	3.7001	409.62	0.151 42
2.6643	381.14	0.414 13	3.9437	409.08	0.272 14
2.8378	385.13	0.403.86	3.6592	409.09	0.146 17
3.0165	389.11	0.390 70	3.9302	408.75	0.278 01
2.4622	389.10	0.071 70	3.6335	408.76	0.143 44
3.2709	394.76	0.371 52	3.9442	409.29	0.267 21
2.7467	394.76	0.083 80	3.6835	409.32	0.148 71
3.5189	399.82	0.350 27	3.9513	409.79	0.253 18
3.0350	399.83	0.097 98	3.7243	409.81	0.154 75
3.6754	402.97	0.333 10	3.9515	410.05	0.242 91
3.2152	402.97	0.109 45	3.7550	410.06	0.158 99
3.8225	406.16	0.309 63	3.9436	410.32	0.230 73
		$x_2 = ($	).6625		
2.3310	357.47	0.438 13	3.9723	391.27	0.320 16
2 4756	361.00	0 429 57	3 4974	391 28	0 111 85
1 8816	361.04	0.046.65	4 1069	393 93	0 295 89
2 6512	364 95	0.499 19	3 7069	303 94	0.126.65
2.0012	264.06	0.051 56	4 1761	205.74	0.120 00
2.0442	369.50	0.001 00	9 9640	305 76	0.209 00
2.8200	300.00	0.411 33	3.0045	390.70	0.140 /0
2.2080	306.72	0.000 04	4.1930	390.17	0.206 33
2.9943	372.34	0.401 23	3.9090	390.18	0.140 82
2.3710	372.37	0.062 18	4.1955	396.43	0.249 84
3.1638	376.00	0.387 68	3.9410	396.44	0.148 94
2.5573	376.00	0.068 66	4.1937	396.73	0.238 41
3.3207	379.04	0.377 92	3.9727	396.75	0.153 40
2.7279	379.05	0.074 72	3.9912	396.92	0.155 69
3.4777	382.09	0.367 34	4.1903	396.96	0.230 02
2.9046	382.11	0.081 67	4.0362	397.37	0.162 77
3.6446	385.18	0.355 30	4.0670	397.56	0.169 18
3.0826	385.19	0.089 81	4,0952	397.68	0.173 71
3,7881	387.85	0.341 30	4.1472	397.83	0.188 59
3.2526	387.86	0.098 33			0.100 00
		*- = (	8109		
2.6508	355.11	0.415.35	4.1291	382.18	0 303 05
2.0000	359 39	0 405 96	3 7950	382.10	A 199 89
2.0071	950 94	0.400 20	4 1800	302.10	0.123 62
2.3013	007.04	0.000 04	4.1002 0 0510	302.11	0.200 00
2.9692	001.00	0.007 21	3.6019	352.77	0.127 37
2.4924 0 1 401	001.00 905 00	0.002 /1	4.1900	JOJ.40	0.266 02
3.1421	365.08	0.386 32	3.9102	383.48	0.132 57
2.6683	365.10	0.068 51	4.2306	384.12	0.279 92
3.3018	368.04	0.377 73	3.9620	384.14	0.137 93
2.8362	368.05	0.074 50	4.2536	384.64	0.270 05
3.4657	370.84	0.367 10	4.0127	384.66	0.143 02
3.0058	370.89	0.081 17	4.2708	385.17	0.259.46
3.6090	373.34	0.356 33	4.0654	385.18	0.149 09
3.1527	373.35	0.087 79	4.2780	385.50	0.246 86
3.7554	375.97	0.346 04	4.1003	385.51	0.154 18

 Table III.
 Neopentane (1) + Propane (2) Data



Figure 2. Pressure-temperature phase diagram for the propane + neopentane system. Dew-bubble curves are for the following mole fractions of propane, right to left: 0.1581, 0.4573, 0.6625, 0.8109, 0.9339. The dashed curve is the fitted critical locus, and the solid curves are the results from the modified Leung-Griffiths correlation.

may be somewhat greater because of the difficulty of measurements in this region.

#### Modified Leung-Griffiths Model

The thermodynamic model first proposed by Leung and Griffiths (8), and subsequently modified by Moldover, Gallagher, and Rainwater (9–13), has proven to be useful in the development of highly accurate VLE correlations of a wide variety of mixtures at high pressures (9–16). The model is explained in detail elsewhere (13); here we simply summarize the equations needed to perform the calculations.

The basic premise of the model, as put forth by Griffiths and Wheeler (93), is that the thermodynamic behavior of mixtures is simpler and more like that of pure fluids if expressed only in terms of field variables. By definition, field variables such as P, T, and the chemical potentials  $\mu_1$  and  $\mu_2$ of fluids 1 and 2 have the same values in coexisting liquid and vapor phases, whereas "density variables" such as x have differing values. Functions of field variables are, of course, also field variables.

P (MPa)	<i>T</i> (K)	$\rho (g/cm^3)$
.8109		
4.2853	385.66	0.238 18
4.1245	385.68	0.156 74
4.2855	385.88	0.227 67
4.1581	385.95	0.162 45
4.1735	386.18	0.168 15
4.2768	386.20	0.212 76
4.2330	386.45	0.180 81
.9339		
4.1268	372.78	0.298 09
4.1622	374.73	0.156 80
4.2543	374.73	0.269 50
4.1988	375.18	0.164 48
4.2722	375.18	0.257 59
4.2319	375.46	0.171 52
4.2927	375.45	0.244 66
4.2531	375.61	0.177 59
4.2654	375.71	0.181 67
4.2936	375.71	0.221 67
4.2871	375.81	0.193 66



Figure 3. Temperature-density phase diagram for the propane + neopentane system. Compositions are the same as in Figure 2. The dashed curve is the fitted critical locus, the upper and lower solid curves are the coexisting density fits for neopentane and propane, respectively, and the intermediate solid curves are the results from the modified Leung-Griffiths correlation.

The independent field variables of the model are

$$\zeta = \frac{e^{\mu_1/RT}}{Ke^{\mu_2/RT} + e^{\mu_1/RT}}$$
(1)

and

$$t = \frac{T - T_{\rm c}(\zeta)}{T_{\rm c}(\zeta)} \tag{2}$$

where  $T_c(\zeta)$  is the mixture critical temperature, R is the gas constant, and K can be a constant or a temperature-dependent function. Since  $\mu_1 \rightarrow -\infty$  for pure fluid 2 (here propane), and vice versa,  $\zeta = 0$  when x = 1 and  $\zeta = 1$  when x = 0. Furthermore, it has been shown (13) that if  $T_c$  is monotonic in x, which is true for mixtures of propane with neopentane and with the hexane isomers, then a function K(T) exists such that x = 1 $-\zeta$  exactly on the critical line. Then there is a unique  $T_c$  for each  $\zeta$ ,  $0 \le \zeta \le 1$ , and eq 2 serves as a definition of t (a dimensionless distance from the critical locus) in terms of  $T_{c}(\zeta)$ .

According to the model, molar densities along loci of constant  $\zeta$  on the coexistence surface are given by

$$\rho = \rho_{\rm c}(\varsigma) [1 \pm C_1(\varsigma)(-t)^{0.355} + C_2(\varsigma)t]$$
(3)

where the plus is used for the liquid and the minus is used for the vapor. In P-T space, loci of constant  $\zeta$  are represented as

$$\frac{P}{T} = \frac{P_{\rm c}(\beta)}{T_{\rm c}(\beta)} [1 + C_3(\beta)(-t)^{1.9} + C_4(\beta)t + C_5(\beta)t^2 + C_6(\beta)t^3]$$
(4)

For  $\zeta = 0$  or 1, the above equations represent fits to the coexisting density curve and the vapor pressure curve of propane or neopentane, respectively. We define  $C_i^{(1)} = C_i(\zeta=1)$  and  $C_i^{(2)} = C_i(\zeta=0)$ , the coefficients of fits to the pure fluid properties. These coefficients are listed in Table IV for propane and neopentane. In previous work (14) an earlier fit (10) to the propane coexistence data of Clegg and Rowlinson (94) was utilized, but it was subsequently found that their liquid densities were significantly lower than those measured in several other independent experiments (95). Accordingly, for propane eqs 3 and 4, with  $\zeta = 0$ , have been refitted to the correlation of Goodwin and Haynes (95). The coefficients for neopentane are based on a fit to the correlation of Das *et al.* (96).

The coexisting mole fractions are calculated according to the relation

$$x = 1 - \zeta \left\{ 1 - \zeta \left[ \frac{\bar{Q}(\zeta,t)}{\rho} - \frac{\bar{Q}(\zeta,t=0)}{\rho_{c}(\zeta)} - \bar{H}(\zeta,t) \right] \right\}$$
(5)

where use of the liquid or vapor density from eq 3 yields the liquid or vapor composition, respectively, and where

$$\bar{Q}(\zeta,t) = \frac{PT_{c}(\zeta)}{RTP_{c}(\zeta)} \frac{d}{d\zeta} \left[ \frac{P_{c}(\zeta)}{T_{c}(\zeta)} \right] + \frac{P_{c}(\zeta)}{RT_{c}(\zeta)} \{C_{3}(\zeta)(-t)^{1.9} + C_{4}(\zeta)t + C_{5}(\zeta)t^{2} + C_{6}(\zeta)t^{3}\} + \frac{P_{c}(\zeta)}{R} \frac{d}{d\zeta} \left[ \frac{1}{T_{c}(\zeta)} \right] (1+t) [-1.9C_{3}(\zeta)(-t)^{0.9} + C_{4}(\zeta) + 2C_{5}(\zeta)t + 3C_{6}(\zeta)t^{2}]$$
(6)

and

$$\bar{H}(\zeta,t) = \frac{1}{T_c(x)} \frac{\mathrm{d}T_c(x)}{\mathrm{d}x} C_{\mathrm{H}}(1+C_{\mathrm{Z}}\zeta)t \tag{7}$$

Equation 7 introduces two adjustable parameters,  $C_{\rm H}$  and  $C_{\rm Z}$ . The  $\zeta$  dependence of  $C_i$  in eq 4 is given by simple linear interpolation between the pure fluids,

$$C_i(\zeta) = C_i^{(2)} + \zeta [C_i^{(1)} - C_i^{(2)}], \quad i = 3-6$$
(8)

whereas the functions of eq 3 are given by the slightly more involved expressions

$$C_{1}(\varsigma) = \frac{C_{1}^{(2)} + \varsigma [C_{1}^{(1)} - C_{1}^{(2)}]}{1 + C_{X}(1 + C_{Y}\varsigma)\varsigma(1 - \varsigma) [\bar{Q}(\varsigma, 0)]/\rho_{c}(\varsigma)}$$
(9)

$$C_2(\zeta) = C_2^{(2)} + \zeta [C_2^{(1)} - C_2^{(2)}] + C_R \zeta (1 - \zeta)$$
(10)

which introduce three more adjustable parameters,  $C_{\rm X}$ ,  $C_{\rm Y}$ , and  $C_{\rm R}$ .

Table IV. Model Parameters for Pure Fluids

	neopentane	propane		neopentane	propane
$\overline{T_{\rm c}({\rm K})}$	433.75	369.85	$C_3$	30.0	29.57
$P_{\rm c}$ (MPa)	3.196	4.247	$C_4$	5.902	5.800
$\rho_{\rm c}  (\rm kmol/m^3)$	3.215	5.001	$C_5$	-24.99	-24.08
$C_1$	1.987	1.958	C <sub>6</sub>	0.0	1.024
$C_2$	-0.83	-0.823			

Table V. Parameters of the Critical Locus

-0.024 979	$\bar{P}_3 (\mathrm{kmol}/\mathrm{m}^3)$	0.037 995
0.005 978	$\tilde{\rho}_1 (\mathrm{kmol/m^3})$	0.260 078
-0.000 867	$\overline{\rho}_2 (\mathrm{kmol/m^3})$	-0.271 430
0.470 937	$\bar{\rho}_3  (\rm kmol/m^3)$	0.127 639
0.021 561		
	-0.024 979 0.005 978 -0.000 867 0.470 937 0.021 561	$\begin{array}{c c} -0.024 \ 979 & \begin{tabular}{l} \hline $P_3$ (kmol/m^3)$\\ 0.005 \ 978 & \begin{tabular}{l} \hline $\rho_1$ (kmol/m^3)$\\ -0.000 \ 867 & \begin{tabular}{l} $\rho_2$ (kmol/m^3)$\\ 0.470 \ 937 & \begin{tabular}{l} $\rho_3$ (kmol/m^3)$\\ 0.021 \ 561 \end{array}$

The critical locus is represented by the following expressions as fitted to the experimentally measured mixture critical points (Table II):

$$\frac{1}{RT_{c}(x)} = \frac{1-x}{RT_{c1}} + \frac{x}{RT_{c2}} + x(1-x)[T_{1} + (1-2x)T_{2} + (1-2x)^{2}T_{3}]$$
(11)

$$x_{\rm T} = \frac{1/T_{\rm c1} - 1/T_{\rm c}(x)}{1/T_{\rm c1} - 1/T_{\rm c2}}$$
(12)

$$\frac{P_{\rm c}(x)}{RT_{\rm c}(x)} = \frac{(1-x_{\rm T})P_{\rm c1}}{RT_{\rm c1}} + \frac{x_{\rm T}P_{\rm c2}}{RT_{\rm c2}} + x_{\rm T}(1-x_{\rm T})[\bar{P}_{\rm 1} + (1-2x_{\rm T})\bar{P}_{\rm 2} + (1-2x_{\rm T})^2\bar{P}_{\rm 3}]$$
(13)

$$\rho_{\rm c}(x) = (1 - x_{\rm T})\rho_{\rm c1} + x_{\rm T}\rho_{\rm c2} + x_{\rm T}(1 - x_{\rm T})[\bar{\rho}_1 + (1 - 2x_{\rm T})\bar{\rho}_2 + (1 - 2x_{\rm T})^2\bar{\rho}_3]$$
(14)

These equations introduce the nine parameters that characterize the critical line,  $T_i$ ,  $\bar{P}_i$ , and  $\bar{\rho}_i$ , i = 1-3. Values of these parameters for the propane + neopentane critical locus are listed in Table V. In some previous correlations (12, 16), the critical locus has been adjusted to optimize the fit to the coexistence surface, thereby causing some disagreement with the mixture critical points as measured and reported by the experimentalist. This procedure is justified in that measurements near or at a critical point are subject to more experimental uncertainty than those removed from the critical locus. For the case of propane + neopentane, a linear least-squares fit to the experimentally measured critical locus yielded an optimal correlation of  $T_c(x)$  and  $P_c(x)$ , but a minor adjustment was needed for  $\rho_c(x)$ .

Table II compares the experimental critical loci to those obtained from the fits of eqs 11–14. The fits reproduce  $T_c(x)$  to within experimental uncertainty and  $P_c(x)$  to within 0.08%, while the optimized fit of  $\rho_c(x)$  is within 1.2% of the experimental values. A diagram of the experimental and fitted critical pressure as a function of composition is given in Figure 4.

The model just described includes, in addition to parameters for the pure fluid coexistence properties and the critical locus, five parameters to characterize the mixture. However, depending on the complexity of the mixture, not all parameters are always needed. A good measure of the complexity of the mixture or overall width of the dew-bubble curves is (12, 13)

$$\alpha_{\rm 2m} = \max[\delta x / (\delta \rho / \rho_c)]$$
(15)

where  $\delta x$  and  $\delta \rho$  are the changes in x and  $\rho$  across the phase boundary in the limit of approach to the critical point. On the basis of studies of a large number of binary mixtures, we have developed the guidelines for nonpolar fluid mixtures



Figure 4. Critical pressure locus for propane + neopentane. The solid curve is the fit according to eqs 12 and 13, and the circles are experimental points.



Figure 5. Pressure-density phase diagram for the propane + neopentane system, for the following mole fractions of propane: ( $\bullet$ ) 0.6625, ( $\Delta$ ) 0.4573, ( $\Delta$ ) 0.1581. The dashed curve is the fitted critical locus. The solid curves are the fitted pure fluid coexistence curves and the results from the modified Leung-Griffiths correlation.

that only  $C_{\rm H}$  is needed if  $\alpha_{\rm 2m} < 0.1$ ,  $C_{\rm H}$  and  $C_{\rm X}$  are needed if  $0.1 < \alpha_{2m} < 0.17$ , and  $C_R$ ,  $C_Y$ , and  $C_Z$  are also needed if 0.17  $< \alpha_{2m} < 0.25.$ 

#### Results

Figures 2 and 3 show the dew-bubble curves as calculated from the modified Leung-Griffiths model and the experimental data. The agreement is excellent, within 0.02 MPa in pressure, 0.3 K in temperature and 8 kg/m<sup>3</sup> in density, with temperature and composition as independent variables, as shown in Figure 3. It is also instructive to examine isopleths on a pressure-density diagram, although because the critical pressure has a maximum, isopleths near that maximum overlap and lead to a cluttered figure. Consequently, in the pressure-density plot of Figure 5, the two dew-bubble curves richest in propane are omitted. With pressure and composition as independent variables, again the densities are correlated to within 8 kg/m<sup>3</sup>, with the largest discrepancies at the highest liquid densities. For these three isopleths, the maxima (maxcondentherm points) in Figure 3 are on the vapor sides, whereas the maxima (maxcondenbar points) in Figure 5 are on the liquid sides.

For this mixture,  $\alpha_{2m} = 0.104$ . As expected for mixtures in the range  $0.1 \le \alpha_{2m} \le 0.17$ , nonzero values for only two of



Figure 6. Fitted critical loci for the mixtures propane + neopentane (18), broken line; propane + isopentane (22), solid line; and propane + n-pentane (50), dashed line.

the five adjustable parameters in eqs 7, 9, and 10 are needed; in particular  $C_{\rm H} = -7$  and  $C_{\rm X} = 0.25$  for propane + neopentane.

Rainwater and Williamson (14) have similarly correlated the VLE data for propane + isopentane of Vaughan and Collins (22),  $\alpha_{2m} = 0.137$ ,  $C_{H} = -6$ ,  $C_{X} = 0.1$ , and Rainwater (13) has correlated the VLE data for propane + n-pentane of Kay and Oxley (50, 52),  $\alpha_{2m} = 0.141$ ,  $C_{\rm H} = -8$ , and  $C_{\rm X} =$ 0.3. The latter correlation is in fair agreement with the data of Sage and Lacey (20) and in good agreement with the data of Vejrosta and Wichterle (21).

Figure 6 shows the critical loci of the mixtures of propane with the three pentane isomers. The maximum critical pressures are 4.302 MPa for the neopentane mixture and 4.575 MPa for both the isopentane mixture and the *n*-pentane mixture. The isopentane mixture data of Vaughan and Collins are rather sparse compared with those of the other two mixtures, so there may be some uncertainty in the parameters for that system. Nevertheless, while each of the propane + pentane mixtures requires only  $C_{\rm H}$  and  $C_{\rm X}$ , there is no obvious trend in the Leung-Griffiths parameters for these mixture correlations.

### Acknowledgment

The authors thank John Lynch and Daniel Friend for assistance with the computer graphics.

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Received for review October 14, 1992. Revised May 20, 1993. Accepted June 8, 1993. J.C.R. was supported in part by the U.S. Department of Energy, Office of Basic Energy Sciences, Division of Chemical Science.